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Generating High Voltage Pulses by Interrupting Current in an Inductive Circuit

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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered) READ INSTRUCTIONS REPORT DOCUMENTATION PAGE BEFORE COMPLETING FORM REPORT NUMBER NRL'Mensorandum Report 3326 ORT & PERIOD COVERED generating high yoltage pulses by Interim repert n a continuing INTERRUPTING CURRENT IN AN INDUCTIVE CIRCUIT NRL problem PERFORMING CRG. REPORT NUMBER CONTRACT OR GRANT NUMBER(+) NUTHORGE M./Friedman MM M./Ur PERFORMING ORGANIZATION NAME AND ADDRESS Playal Research Laboratory Washington, D.C. 20375 11 CONTROLLING OFFICE NAME AND ADDRESS 12. REPORT DATE July 76 DESTRUCT PAGES 14 TA. MONITORING AGENCY NAME & ADDRESS(II different from Co ontrolling Office) 15. SECURITY CLASS. (of this report) UNCLASSIFIED 18a. DECLASSIFICATION/DOWNGRADING 16 DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. 17 DISTRIBUTION STATEMEN? (of the abstract entered in Block 20, If different from Report) 18. SUPPLEMENTARY NOTES *M. Ury's present address is Fusion Systems Co., Rockville, Maryland. 19 KEY NORDS (Continue on reverse eide if necessary and Wastify by block number) Inductive store Orening switch High power ABRITRACT (Continue on reverse side if necessory and identify by black number) A new approach to the problem of developing an opening switch for inductive systems is described. The switch (fuse) consists of an Aumini m foll immersed in water. Heat transfer processes and chemical reactions between the AX and water determine switch performance. Six kilojoules of electrical energy was handled by the switch and voltages or up to 100 kV were generated across the switch electrodes.

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GENERATING HIGH VOLTAGE PULSES BY INTERRUPTING CURRENT IN AN INDUCTIVE CIRCUIT

Possible needs for high power electrical pulses with energy greater than 10 MJ¹ lead to a re-examination of the concept of inductive storage systems. In such systems, electrical energy is stored efficiently in an inductor, L, through which current is flowing. The energy is switched into a load by opening a switch in series with the inductor. This causes an interruption in current and therefore a voltage is generated across the switch. A switch must be able to withstand very high inductive voltages to rapidly "discharge" a large inductive energy store. A possible opening switch commonly employed consists of a metallic wire or foil type fuse. When sufficient electrical energy is dissipated in the fuse, it explodes and the resistance can increase by orders of magnitude. This change in the electrical properties of the fuse causes the desired current discontinuity. When a capacitor bank is used to "charge" an inductive store the relative performance of a switch can be measured by a quality factor α which includes the relevant parameters of interest:

$$\alpha = \frac{t_{c}}{\sqrt{T_{1/2} \left(\frac{L}{R_{m}}\right)}},$$
 (1)

Note: Manuscript submitted July 7, 1976.

where t_c is the charging time of the inductor prior to fuse explosion, $T_{1/2}$ is the width of the resultant voltage pulse, and R_m is the resistance of the cwitch at the maximum voltage. A value of α as high as 10 has been reported, but only at output voltages of 12 kV.

We report here on an improved opening switch. Values of $\alpha \ge 30$ were obtained and voltages of 100 kV generated across the opened switch. Figure 1 shows the experimental arrangement. A capacitor bank, C = 300 μ F, was connected to either a 12.250 or 400 μ H inductor, L. A metallic foil or fuse, immersed in a demineralized water bath, completed the electrical circuit. A Rogovsky coil and a resistive divider measured the current flowing in the system and the voltage developed across the foil. Aluminum foils of various length, ℓ , thickness, ℓ , and width, ℓ , were used. In addition, Mg, Ag, Au, Cu, and Ta foils were also used. Figure 2 shows typical current and voltage traces for a reasonably optimal choice of A ℓ foil.

Since α depends on R_m it is obvious that a greater value of ℓ gives larger values of R_m and α . For example, Fig. 3 shows the dependence of α on ℓ . Figure 4 gives the current, voltage, resistance and power dissipation as a function of time for two values of $L(V_0 \approx 6.6 \text{ kV})$. The performance of different materials used as a switch foil was judged from the value of α and was found to be: $A\ell$, Mg, Ag, Au, and Ta (in a descending order).

Four different Al foils with the same cross-sectional area were tested. Each of them had a different width and thickness. Figure 5 shows the voltage developed along each of these fuses. When a very wide

foil was used (Fig. 5a) the fuse never reached high values of resistance and voltage. When the foil resembled a wire (Fig. 5b) the resistance reached initially a high value but immediately dropped (restrike). When foils used were of width which fell between the previous two extremes (Fig. 5c and 5d), resistance and voltage reached and maintained high values.

The switch performance was improved when hydrogen peroxide $(\frac{1}{2}\frac{0}{2})$ was added to the water immersing the switch. For example an increase in voltage by a factor of two was observed when 70% H 0 was used.

Relationships developed by Maisonnier, et al.4 for the condition of foil vaporization at peak current, define a foil cross-sectional area, s, as:

$$s = w\delta = \left(\frac{\left(\frac{1}{2} c v_o^2\right)^{3/2}}{v_o L^{1/2} k_1 a}\right)^{1/2}, \qquad (2)$$

where a is a constant characteristic of the material of the foil and $1 < k_1 < 3$. Reference (4) does not explain the behavior of the fuse after vaporization, especially the time behavior of the resistance. The experimental results described earlier suggest that mechanisms other than ohmic heating may play an important role when a metallic foil is exploded under water. We speculate that two processes in addition to the ohmic heating have to be considered: (1) a heat loss from the foil to the water and (2) a chemical reaction between the material of the fuse and the water. In that case the internal energy of the foil, e, is governed

by an equation of the form

$$m \frac{de}{dt} \approx q_1 + q_2 - q_3 , \qquad (3)$$

where q is the rate of ohmic heating

$$q_1 = I^2 \frac{\rho(T)\ell}{w \delta} , \qquad (4)$$

 $\rho(T)$ is the resistivity of the foil at temperature T, η_2 is the rate of chemical heating and is proportional to

$$q_p \sim w \ell T^{1/2} \exp(-A/T) . \qquad (5)$$

This dependence was obtained from kinetic theory. The parameter A depends on the threshold temperature of the reaction. For example the threshold temperature of the reaction

$$2 Al + 3 H_0 \rightarrow Al_{23} + 3 H_2$$
 (6)

is about 700°C. The chemical reaction rate of energy gain, q₂, depends on the energy released by the chemical reaction. The higher the energy released the larger q₂ is. The interaction described by Eq. (6) gives 15 kJ/gm. Less energy is released when Mg, Cu, Ag, and Au are used (in a descending order). The quantity q₃ (Eq. 4) is the rate of heat loss to water and is given approximately by

$$q_3 \approx \lambda \frac{dm}{dr} \approx \lambda 2 \rho_d w \ell V_s$$
, (7)

where λ is the heat of vaporization of water, m is the mass of water vaporized, $\rho_{\bf d}$ is the density of water and V is the escape velocity of steam bubbles from the foil. If one assumes that the force which ejects the steam bubbles from the foil depends on gas pressure within the bubble and that only viscous forces oppose the motion of the bubbles in the liquid than $V_{\bf s} \sim T$ or $q_{\bf s} \sim w \ell T$.

Each of the above processes can be predominant during different times of the current cycle. At the initial stage when R and I both increase with time $q_1 > q_2$ and $q_3 \approx 0$. At a certain time the current does not change very much and the resistance stays constant (although tha temperature of the foil increases). Since q ~ wlT it is possible by choosing a large w (and a small δ) to increase q_{α} without changing q_{γ} and to have $\textbf{q}_{_{3}} \approx \textbf{q}_{_{1}}$. This will define an "equilibrium" temperature, $\textbf{T}_{_{1}}$. If T is below the temperature of foil vaporization and $q_{\rm p}\approx 0$ no explosion will occur and the energy in the inductive store will dissipate gently into the water (Fig. 5a). If T is above the ignition point of the chemical reaction then $q_{_{\mathcal{D}}} > 0$. In that case the temperature of the fuse will increase. Since $q_2 \sim w \ell \sqrt{T}$ and $q_3 \sim w \ell T$ (for large T) the foil will reach an "equilibrium" temperature T_p for which $q_1 + q_p \approx q_q$. If T is below the temperature for which ionization occurs the foil will change its characteristics from a conductor (e.g. Al) to an insulator (e.g. Al 0) and a successful switching will occur (Fig. 5c and 5d). If w is small so that q_3 is always smaller than $\frac{1}{2}$ the temperature of the fuse will increase to a value for which ionization may start (Fig. 5b).

In order to convert the conductor to an insulator as fast as possible, the chemical reaction has to rapidly supply a lot of energy. The amount of energy released depends on the material of the fuse. The ranking of such materials (based on the chemical reaction released) is Al, Mg, Cu, Ag and Au (in a decending order). This is exactly the same ranking obtained experimentally based on the switch quality factor α . Moreover, by using Al foil immersed in H 0 more chemical energy can be released with an improved switch performance.

In summary, experiments have shown that thin Al foils immersed in water have improved characteristics as fuses in an inductive circuit.

The improvement may possibly be due to the process of heat losses through the water bath, and a chemical reaction of the Al foil with water.

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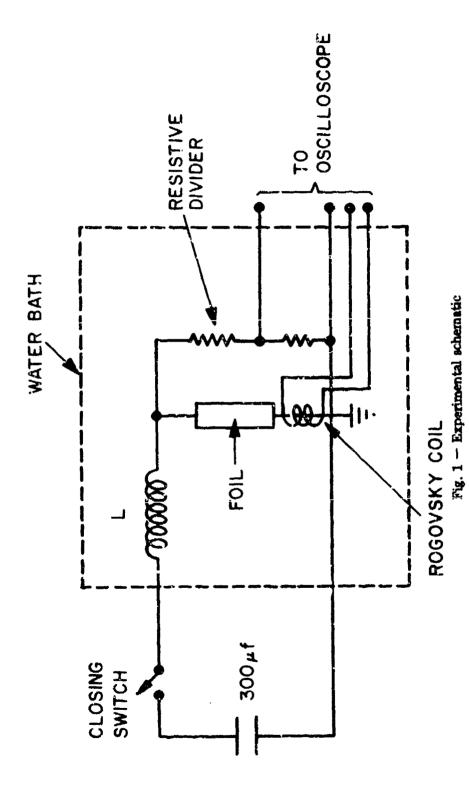
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- 6. The quality factors α for Al, Mg, Cu, Ag, and Au were 40:20:10:8:7 respectively and were obtained under the same conditions (V = 6.6 kV, L = 12 μ H, ℓ = 25 cm).

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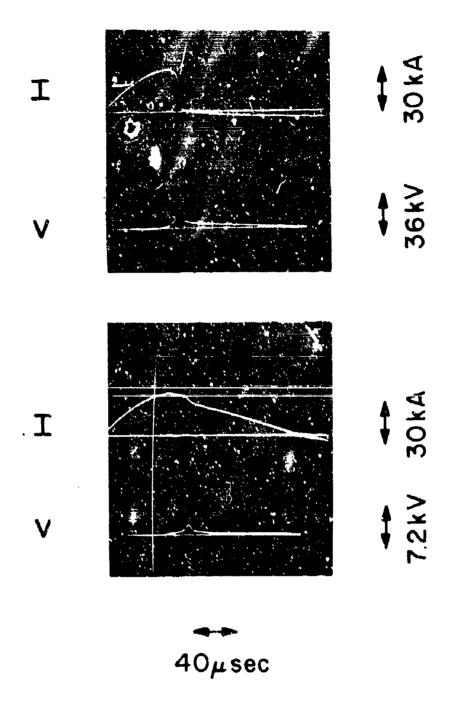


Fig. 2 — Traces of the current flowing through the system and the voltage developed along the switch for A^{ℓ} foil in water (top) and in air (bottom) [$\ell = 25$ cm, $\delta = 2.5 \times 10^{-3}$ and w = 2.5 cm]. The inductance L was 12 μ H and the voltage on the capacitor bank, V_{o} , was 6.6 kV.

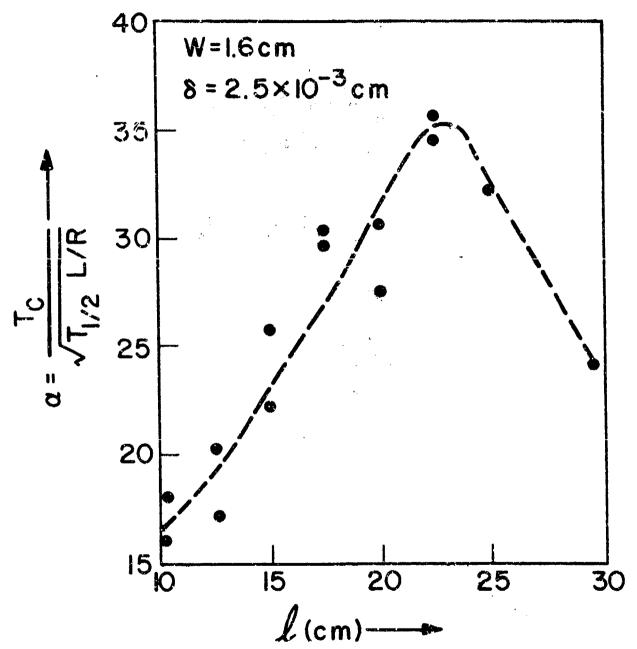


Fig. 3 — The dependence of α on the length of the Al foil

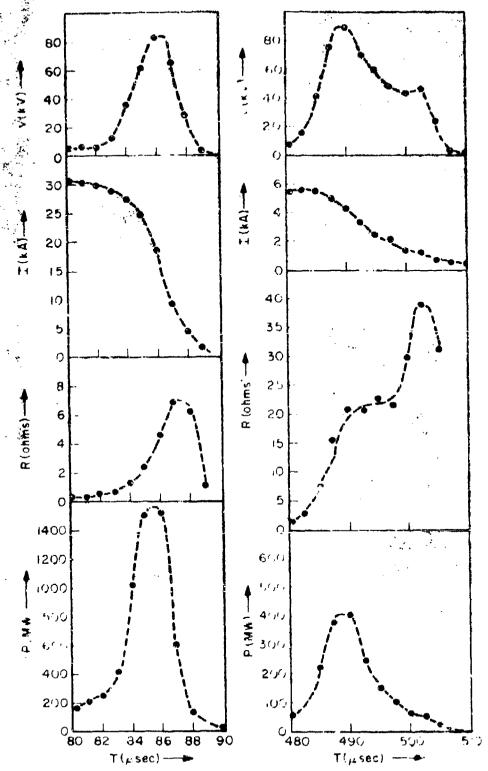


Fig. 4 — Voltage, current, resistance and power vs time for [these results were obtained using Al] (1) (left) L = 12 μ H; V_o = 6.6 kV; w = 2.5 cm; δ : 2.5 × 10⁻⁸ cm; ℓ = 22.5 cm and (2) (right) L = 400 μ H; V_o = 6.6 kV; w = 1.6 cm; δ = 0.5 × 10⁻⁸ cm; ℓ = 83 cm

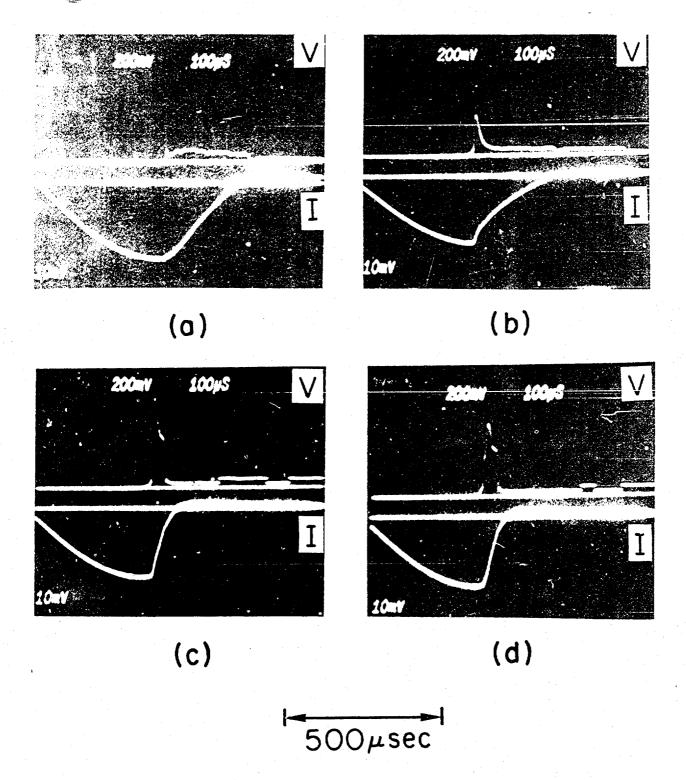


Fig. 5 - Traces of the current flowing through the system and the voltage that developed along the Al foil in water

- (a) $\ell = 37$ cm, w = 7.8 cm, $\delta \approx 0.5 \times 10^{-3}$ cm
- (b) $\ell = 37$ cm, w = 0.4 cm, $\delta \approx 9.4 \times 10^{-3}$ cm (c) $\ell = 37$ cm, w = 1.5 cm, $\delta \approx 2.5 \times 10^{-3}$ cm

(d) ℓ = 37 cm, w = 2.1 cm, $\delta \approx 1.8 \times 10^{-3}$ cm. The traces were obtained for L \approx 250 μ H and V = 6.6 kV.